

UNIT - III

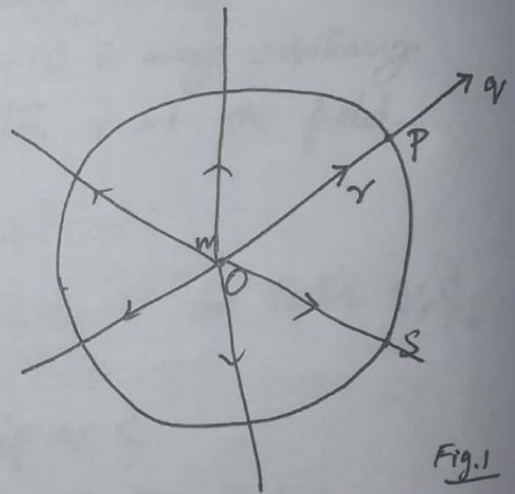
Sources, Sinks and Doublets (Three-dimensional Hydrodynamical Singularities)

Source: An outward Symmetrical radial flow in all directions is termed as a three dimensional Source or a Simple Source.

(or)

Suppose at a point O in a fluid the flow is such that it is directed radially outwards from O in all directions and in a Symmetrical manner. Then fluid enters the System through O which is termed a Simple Source.

Sink: If at O the volume entering per unit time is $4\pi m$, where m is a constant, then the strength of the Source is defined to be m .



If however, the flow is such that fluid is directed radially inwards to O from all directions in a Symmetric manner, then fluid leaves the System at O which is termed a Simple Sink.

A Sink of strength m is a Source of strength $-m$.

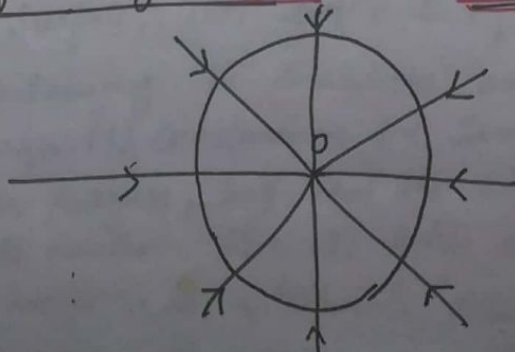


Fig. 1. Shows a

Simple source of strength m at O in a fluid which is presumed to contain no other sources or sinks and which would otherwise be at rest.

B.W.: Velocity of a fluid Particle at due to source of strength m .
 S is the Surface of the Sphere centre, O and radius r and P is a field on S such that $\overline{OP} = r$.

Then the fluid velocity at P is \bar{q} along \overline{OP} and magnitude q is everywhere constant over S .

The volume of fluid crossing S per unit time is $4\pi r^2 q$;

that emitted from O per unit time is $4\pi m$.

\therefore the fluid is incompressible, these two are equal from considerations of continuity.

$$4\pi r^2 q = 4\pi m$$

$$q = \frac{m}{r^2}$$

(Sink velocity)

$$\bar{q} = \frac{m}{r^2} \hat{r}$$

(in vector form)

$\rightarrow (1)$

It is easily shown that $\nabla \times \bar{q} = 0$ (except at $r=0$)

so that flow is of the potential kind.

Let ϕ be the velocity potential at P .

$$\text{let } \phi = \phi(r), \quad \partial_r$$

$$\nabla \phi = \phi'(r) \hat{r} \quad \rightarrow (2)$$

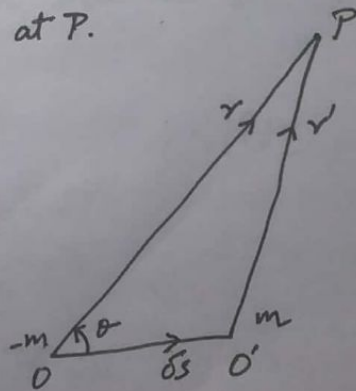
$$\text{Thus } \bar{q} = -\nabla \phi \Rightarrow \nabla \phi = -\bar{q} \quad \rightarrow (3)$$

From (2) & (3), using (3),

$$\phi'(r) = -\frac{m}{r^2}$$

Integrating,

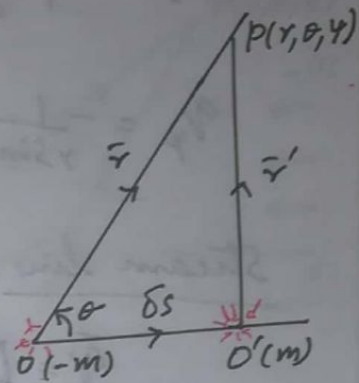
$$\phi(r) = -m \left(-\frac{1}{r} \right) = \frac{m}{r}$$



Book work: Velocity potential due to doublet at $P(r, \theta, \psi)$

The Velocity potential ϕ at $P(r, \theta, \psi)$ due to the doublet at O .

Let, the flow to be entirely due to $-m$ at O and m at O' .



The velocity Potential at P is $\phi = \frac{-m}{OP} + \frac{m}{O'P}$

$$\phi = \frac{m}{r'} - \frac{m}{r} = \frac{m(r-r')}{rr'}$$

$$\because \overline{OP} - \overline{O'P} = \overline{OO'} \\ r - r' = \delta s$$

$$= \frac{m \cdot \delta s}{rr'} \cdot \frac{r+r'}{r+r'}$$

$$= m \delta s \left(\frac{r+r'}{rr'(r+r')} \right)$$

$$= M \left(\frac{r+r'}{rr'(r+r')} \right)$$

$$\therefore m \delta s = M$$

Let O - fixed

$O' \rightarrow O$

$r' \rightarrow r$

$M \rightarrow \text{Constant}$. Then in the limit we have

$$\phi = M \left(\frac{2r}{r \cdot r(2r)} \right) = M \cdot r^{-2} = (M \cdot r) r^{-3}$$

with $\angle POO' = \theta$,

$$\phi = (M \cdot \hat{r}) \cdot r^{-2}$$

(other equivalent forms for ϕ)

$$= \frac{|M| |\hat{r}| |\cos \theta|}{r^2}$$

$$\because |\hat{r}| = 1$$

$$\phi = \frac{M \cdot \cos \theta}{r^2}$$

The Velocity components at P , are

$$v_r = -\frac{\partial \phi}{\partial r} = -M \cos \theta \left(\frac{-2}{r^3} \right) = \frac{2M \cos \theta}{r^3}$$

$$q_\theta = -\frac{1}{r} \frac{\partial \phi}{\partial \theta} = -\frac{1}{r} \left(-\frac{M \sin \theta}{r^2} \right) = \frac{M \sin \theta}{r^3}$$

$$q_r = -\frac{1}{r \sin \theta} \frac{\partial \phi}{\partial r} = -\frac{1}{r \sin \theta} (0) = 0$$

Stream line:

$$\vec{q} = [q_r, q_\theta, q_\psi] = \left[\frac{2M \cos \theta}{r^3}, \frac{M \sin \theta}{r^3}, 0 \right]$$

The equation of stream lines are

$$\frac{dr}{q_r} = \frac{r d\theta}{q_\theta} = \frac{r \sin \theta dr}{q_\psi}$$

$$\frac{dr}{\frac{2M \cos \theta}{r^3}} = \frac{r d\theta}{\frac{M \sin \theta}{r^3}} = \frac{r \sin \theta dr}{0}$$

Comparing ratio I & II,

$$\frac{dr}{\frac{2M \cos \theta}{r^3}} = \frac{r d\theta}{\frac{M \sin \theta}{r^3}}$$

$$\frac{dr}{r} = \frac{2 \cos \theta}{\sin \theta} d\theta \Rightarrow \frac{dr}{r} = 2 \cot \theta d\theta$$

Integrating,

$$\log r = 2 \log \sin \theta + \log c$$

$$= \log \sin^2 \theta + \log c$$

$$\log r = \log c \sin^2 \theta$$

$$\boxed{r = c \sin^2 \theta}$$

III ratio,

$$d\psi = 0$$

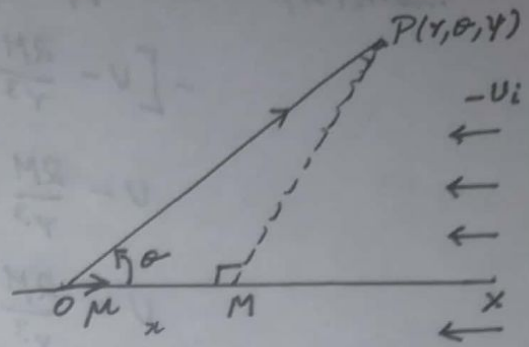
Integrating

$$\boxed{\psi = \text{Constant}}$$

(\because denominator $= 0$)

1) Doublet in an uniform stream

Figure shows a doublet of vector moment $M = \mu_i$ at O in a uniform stream.



Velocity (in the absence of the doublet) = $-U_i$

Find the Velocity Potential $\phi(r, \theta)$ at $P(r, \theta, \psi)$ in the fluid → Spherical Polar Coordinates

If $PM \perp$ from P on OX

if $OM = x$, then the velocity Potential at P due to the streamline $U_x = U r \cos \theta$

$$\text{Due to the doublet at } O = \frac{M \cos \theta}{r^2}$$

∴ The total velocity potential at P is

$$\phi = Ux + \frac{M \cos \theta}{r^2}$$

$$= U r \cos \theta + \frac{M \cos \theta}{r^2}$$

$$= (U r + M r^{-2}) \cos \theta \quad \rightarrow (1)$$

The velocity component at P are

$$q_r = -\frac{\partial \phi}{\partial r} = -\left(U - \frac{2M}{r^3}\right) \cos \theta \quad \rightarrow (2)$$

$$q_\theta = -\frac{1}{r} \frac{\partial \phi}{\partial \theta} = -\frac{1}{r} (U r + M r^{-2}) (-\sin \theta)$$

$$= \frac{1}{r} U + \frac{M}{r^3} \quad \rightarrow (3)$$

$$q_\psi = -\frac{1}{r \sin \theta} \frac{\partial \phi}{\partial \psi} = -\frac{1}{r \sin \theta} (0) = 0 \quad \rightarrow (4)$$

From (2), Also $q_r = 0$

$$-\left[U - \frac{2M}{r^3}\right] \cos \theta = 0$$

$$U - \frac{2M}{r^3} = 0$$

$$U = \frac{2M}{r^3}$$

$$r = \left(\frac{2M}{U}\right)^{1/3}$$

$$-\cos \theta = 0$$

$$\cos \theta = 0$$

$$\theta = \cos^{-1}(0)$$

$$\theta = \frac{\pi}{2}$$

It follows that there is no flow over the surface of the sphere $r=a$

$$\therefore q_r = 0 \text{ at } r=a$$

(2) In $r \geq a$, with $U - \frac{2M}{a^3} = 0$

$$\frac{2M}{a^3} = U$$

$$M = \frac{Ua^3}{2}$$

Sub. in eqn. (2), we get, the same velocity potential as was obtained for uniform flow past a stationary sphere of radius 'a'.

The region $r \geq a$,

the analysis of this sphere problem is the same as that of the dipole of the sphere $\frac{1}{2}Ua^3$ in the uniform stream of velocity $-U_i$, the axis of the dipole being in the direction of i .

Example

1. Illustration of line distribution

Prove that the Velocity potential at a point P due to a uniform finite line source AB of strength m per unit length is of the form $\phi = m \log f$, where

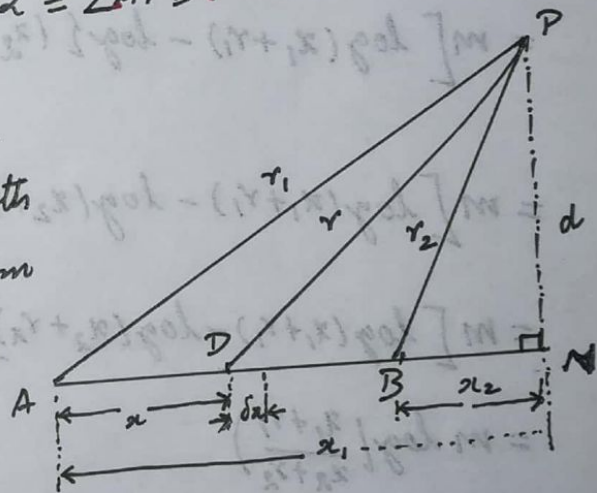
$$f = \frac{r_2 + x_2}{r_1 + x_1} = \frac{r_1 - x_1}{r_2 - x_2} = \frac{a+l}{a-l}$$

in which $AB = 2l$, $PA = r_1$, $PB = r_2$, $NA = x_1$, $NB = x_2$, N being the foot of the perpendicular from P on the line AB , and $2a$ the length of the major axis of the Spheroid through P having A, B as foci.

Show that the Velocity at P is $\frac{(2ml \cos \alpha)}{(a^2 - l^2)u}$, where u is the unit vector along the normal to the Spheroid at P and $2\alpha = \angle APB$.

Sol. ~~Let P be any point on~~

The line section of length δx in AB at distance x from A is effectively a point source of strength $m \delta x$ giving a velocity potential at P of amount $\frac{m \delta x}{r}$



where $AP = r_1$, $AM = x_1$, $BM = x_2$, where AM is the orthogonal projection of AP on AB . Also let $PN = d$, $AP = r_1$, $BP = r_2$.

From elementary geometry,

$$\begin{aligned} PD^2 &= DN^2 + PN^2 \\ r^2 &= (x_1 - x)^2 + d^2 \\ &= (x_1 - x)^2 + (r_1^2 - x_1^2) \end{aligned}$$

The total velocity potential at P due to the entire line distribution AB ($=2l$) is

$$\phi = \int_0^{2l} \frac{m dx}{r} \quad \text{--- (1)}$$

$$\phi = m \int_0^{2l} \frac{dx}{\sqrt{(x_1-x)^2 + (r_1^2-x_1^2)}} \quad \left(\dots \int_x^\beta \frac{1}{\sqrt{x^2+a^2}} dx \right)$$

$$= m \left[\log \left\{ \frac{(x_1-x) + \sqrt{(x_1-x)^2 + (r_1^2-x_1^2)}}{-1} \right\} \right]_0^{2l} = \left[\log(x + \sqrt{x^2+a^2}) \right]_x^\beta$$

$$= m \left[\log \left\{ (x_1-x) + \sqrt{(x_1-x)^2 + (r_1^2-x_1^2)} \right\} \right]_{2l}^0$$

$$= m \left[\frac{1}{2} \log \left\{ r_1 + \sqrt{r_1^2 + r_1^2 - x_1^2} \right\} - \log \left\{ (x_1-2l) + \sqrt{(x_1-2l)^2 + (r_1^2-x_1^2)} \right\} \right]$$

$$= m \left[\log(x_1+r_1) - \log \left\{ (x_2-x_1) + \sqrt{x_2^2+r_1^2-x_1^2} \right\} \right]$$

$$(\because x_1-2l = x_1-AB = x_2)$$

$$= m \left[\log(x_1+r_1) - \log(x_2 + \sqrt{r_2^2}) \right]$$

$$= m \left[\log(x_1+r_1) - \log(x_2+r_2) \right]$$

$$\text{where } r_1^2 - x_1^2 = d^2 = r_2^2 - x_2^2$$

$$= m \log \left(\frac{x_1+r_1}{x_2+r_2} \right)$$

Again, the relation $r_1^2 - x_1^2 = r_2^2 - x_2^2$

$$(r_1 - x_1)(r_1 + x_1) = (r_2 - x_2)(r_2 + x_2)$$

\Rightarrow

$$\frac{r_1+x_1}{r_2+x_2} = \frac{r_2-x_2}{r_1-x_1} = \frac{r_1+r_2+x_1-x_2}{r_1+r_2-x_1+x_2}$$

$$= \frac{r_1+r_2+2l}{r_1+r_2-2l}$$

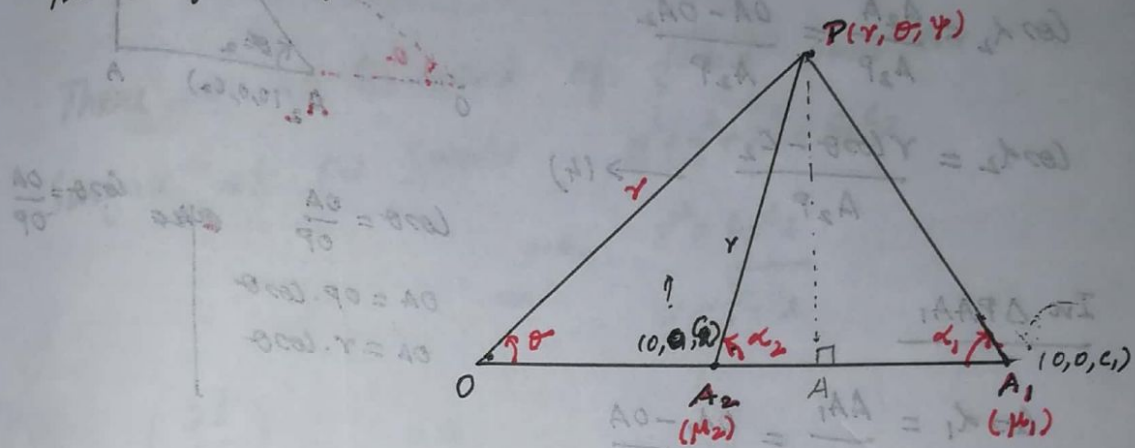
$$\text{Thus, } \phi = m \log \left(\frac{r_1+r_2+2l}{r_1+r_2-2l} \right) = m \log \left(\frac{a+l}{a-l} \right)$$

where $2a$, is the length of major axis of the ellipsoid of revolution through P having A and B as foci since for such an ellipsoid.

$$r_1 + r_2 = \text{constant}$$

It follows from here that the equipotential surfaces $\phi = \text{constant}$ are precisely the family of confocal ellipsoid $r_1 + r_2 = 2a$ obtained when 'a' is allowed to vary.

2). Doublet of strength M_1, M_2 are situated at Point A_1, A_2 whose Cartesian coordinates are $(0, 0, c_1), (0, 0, c_2)$ their axes being ~~direction~~ directed towards and away from the origin respectively. Find the condition that there is no transport of fluid over the surface of the sphere $x^2 + y^2 + z^2 = c_1 c_2$.



velocity potential due to doublet

$$\phi = \frac{M \cos \theta}{r^2}$$

Let OA_2A_1 be the initial line

Let $P(r, \theta, \psi)$ has spherical polar coordinates & be any point in the fluid.

The axes of the doublets at A_1, A_2 make angles α_1, α_2 with A_1P, A_2P . Then the Velocity Potential at

P is

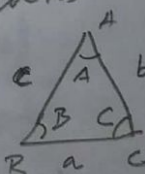
$$\phi = \frac{M_2 \cos \alpha_2}{A_2P^2} + \frac{M_1 \cos \alpha_1}{A_1P^2} \quad \rightarrow (1)$$

By applying Cosine formula ($a^2 = b^2 + c^2 - 2bc \cos A$)

In $\triangle OA_1P$

$$(A_1P)^2 = (OP)^2 + (OA_1)^2 - 2(OP)(OA_1) \cos \theta$$

$$(A_1P)^2 = r^2 + c_1^2 - 2rc_1 \cos \theta \quad \rightarrow (2)$$



In $\triangle OA_2P$

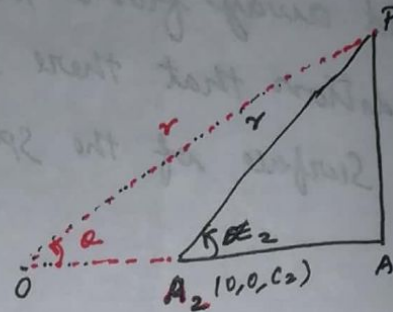
$$(A_2P)^2 = (OP)^2 + (OA_2)^2 - 2(OP)(OA_2) \cos\theta$$

$$(A_2P)^2 = r^2 + c_2^2 - 2rc_2 \cos\theta \quad \rightarrow (3)$$

In $\triangle PA_2A$

$$\cos \alpha_2 = \frac{A_2A}{A_2P} = \frac{OA - OA_2}{A_2P}$$

$$\cos \alpha_2 = \frac{r \cos\theta - c_2}{A_2P} \quad \rightarrow (4)$$



$$\cos\theta = \frac{OA}{OP} \quad \cos\theta = \frac{OA}{OP}$$

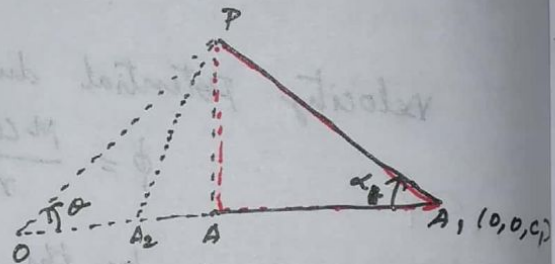
$$OA = OP \cdot \cos\theta$$

$$OA = r \cdot \cos\theta$$

In $\triangle PA_1A$

$$\cos \alpha_1 = \frac{AA_1}{A_1P} = \frac{OA_1 - OA}{A_1P}$$

$$= \frac{c_1 - r \cos\theta}{A_1P} \quad \rightarrow (5)$$



Sub. (2), (3), (4) & (5) in (1) we get

$$\phi = \frac{M_1 (c_1 - r \cos\theta)}{(A_1P) (\gamma^2 + c_1^2 - 2\gamma c_1 \cos\theta)} + \frac{M_2 (r \cos\theta - c_2)}{(A_2P) (\gamma^2 + c_2^2 - 2\gamma c_2 \cos\theta)}$$

$$= \frac{M_1 (c_1 - r \cos\theta)}{(\gamma^2 + c_1^2 - 2\gamma c_1 \cos\theta)^{1/2} (\gamma^2 + c_1^2 - 2\gamma c_1 \cos\theta)} + \frac{M_2 (r \cos\theta - c_2)}{(\gamma^2 + c_2^2 - 2\gamma c_2 \cos\theta)^{1/2} (\gamma^2 + c_2^2 - 2\gamma c_2 \cos\theta)}$$

$$\phi = M_1 (c_1 - r \cos\theta) (\gamma^2 + c_1^2 - 2\gamma c_1 \cos\theta)^{-3/2} + M_2 (r \cos\theta - c_2) (\gamma^2 + c_2^2 - 2\gamma c_2 \cos\theta)^{-3/2}$$

$$\frac{\partial \phi}{\partial r} = M_1 \left\{ (c_1 - r \cos \theta) \left(-\frac{3}{2}\right) (r^2 + c_1^2 - 2rc_1 \cos \theta)^{-5/2} \right. \\ \left. (2r - 2c_1 \cos \theta) + (r^2 + c_1^2 - 2rc_1 \cos \theta)^{-3/2} (-\cos \theta) \right\} \\ + M_2 \left\{ (r \cos \theta - c_2) \left(-\frac{3}{2}\right) (r^2 + c_2^2 - 2rc_2 \cos \theta)^{-5/2} \right. \\ \left. (2r - 2c_2 \cos \theta) + (r^2 + c_2^2 - 2rc_2 \cos \theta)^{-3/2} \cos \theta \right\}$$

There is no transport of fluid over the surface of the sphere, $x^2 + y^2 + z^2 = c_1 c_2$

$$\text{i.e., } r^2 = c_1 c_2 \\ r = \sqrt{c_1 c_2}$$

$$\left(\frac{\partial \phi}{\partial r} \right)_{r=\sqrt{c_1 c_2}} = 0$$

$$\left[M_1 \left\{ (c_1 - r \cos \theta) \left(-\frac{3}{2}\right) (r^2 + c_1^2 - 2rc_1 \cos \theta)^{-5/2} (2r - 2c_1 \cos \theta) \right. \right. \\ \left. \left. + (r^2 + c_1^2 - 2rc_1 \cos \theta)^{-3/2} \cos \theta \right\} \right. \\ \left. + M_2 \left\{ (r \cos \theta - c_2) \left(-\frac{3}{2}\right) (r^2 + c_2^2 - 2rc_2 \cos \theta)^{-5/2} (2r - 2c_2 \cos \theta) \right. \right. \\ \left. \left. + (r^2 + c_2^2 - 2rc_2 \cos \theta)^{-3/2} \cos \theta \right\} \right]_{r=\sqrt{c_1 c_2}} = 0 \\ - M_1 \left\{ (c_1 - \sqrt{c_1 c_2} \cos \theta) \left(-\frac{3}{2}\right) (c_1 c_2 + c_1^2 - 2c_1^{3/2} c_2^{1/2} \cos \theta)^{-5/2} (2\sqrt{c_1 c_2} - 2c_1 \cos \theta) \right. \\ \left. - (c_1 c_2 + c_1^2 - 2c_1^{3/2} c_2^{1/2} \cos \theta)^{-3/2} \cos \theta \right\} \\ + M_2 \left\{ (\sqrt{c_1 c_2} \cos \theta - c_2) \left(-\frac{3}{2}\right) (c_1 c_2 + c_2^2 - 2c_2^{3/2} c_1^{1/2} \cos \theta)^{-5/2} (2\sqrt{c_1 c_2} - 2c_2 \cos \theta) \right. \\ \left. + (c_1 c_2 + c_2^2 - 2c_2^{3/2} c_1^{1/2} \cos \theta)^{-3/2} \cos \theta \right\} = 0 \\ \Rightarrow M_2 \left[\cos \theta \left\{ c_1 c_2 - 2(c_1 c_2)^{1/2} c_2 \cos \theta + c_2^2 \right\}^{-3/2} - 3 \left\{ (c_1 c_2)^{1/2} \cos \theta - c_2 \right\} \right. \\ \left. \left\{ c_1 c_2 - 2c_2 (c_1 c_2)^{1/2} \cos \theta + c_2^2 \right\}^{-5/2} + \left\{ (c_1 c_2)^{1/2} - c_2 \cos \theta \right\} \right] \\ = M_1 \left[\cos \theta \left\{ c_1 c_2 - 2(c_1 c_2)^{1/2} c_1 \cos \theta + c_1^2 \right\}^{-3/2} + 3 \left\{ c_1 - (c_1 c_2)^{1/2} \cos \theta \right\} \right. \\ \left. \left\{ c_1 c_2 - 2c_1 (c_1 c_2)^{1/2} \cos \theta + c_1^2 \right\}^{-5/2} + \left\{ c_1 - (c_1 c_2)^{1/2} \cos \theta \right\} \right]$$

$$\frac{M_2}{M_1} = \frac{\cos\theta C_1^{-3/2} \left[C_2 - 2\sqrt{C_1 C_2} \cos\theta + C_1 \right]^{-3/2} + 3C_2^{1/2} (C_2^{1/2} - C_1^{1/2} \cos\theta) C_1^{-5/2} (C_2 - 2\sqrt{C_1 C_2} \cos\theta + C_2)^{5/2}}{C_1^{1/2} (C_2^{1/2} - C_1^{1/2} \cos\theta)}$$

$$\frac{\cos\theta C_2^{-3/2} (C_1 - 2\sqrt{C_1 C_2} \cos\theta + C_2)^{-3/2} + 3C_2^{1/2} (C_2^{1/2} - C_1^{1/2} \cos\theta) C_2^{-5/2} (C_1 - 2\sqrt{C_1 C_2} \cos\theta + C_2)^{5/2}}{C_2^{1/2}}$$

$$\Rightarrow \frac{M_2}{M_1} = \frac{C_1^{-3/2}}{C_2^{-3/2}}$$

$$\Rightarrow \frac{M_2}{M_1} = \left(\frac{C_2}{C_1} \right)^{3/2}$$

$$0 = \left(\frac{\partial \phi}{\partial \theta} \right)$$

1. Prove that the Velocity potential at a point P due to a uniform finite line source AB of strength m per unit length is of the form $\phi = m \log t$, where

$$t = \frac{r_2 + x_2}{r_1 + x_1} = \frac{r_1 - x_1}{r_2 - x_2} = \frac{a+l}{a-l}$$

in which $AB = 2l$, $PA = r_1$, $PB = r_2$, $NA = x_1$, $NB = x_2$,

N being the foot of the perpendicular from P on the line AB , and $2a$ the length of the major axis of the Spheroid through

P having A, B as foci.

Show that the Velocity at P is $\frac{2ml \cos \alpha}{a^2 - l^2} \hat{u}$, where u is the unit vector along the normal to the Spheroid at P and

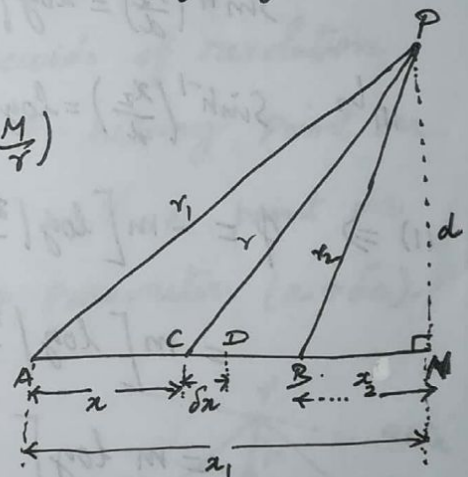
$$2\alpha = \angle APB$$

Sol: The line section of length $CD = \delta x$ in AB at distance x from A is effectually a point source $m\delta x$ giving a Velocity Potential at P is

$$\phi = \frac{m\delta x}{r} \quad (\because \phi = \frac{M}{r})$$

In $\triangle PCN$

$$\begin{aligned} r^2 &= d^2 + CN^2 \\ &= d^2 + (AN - AC)^2 \\ &= d^2 + (x_1 - x)^2 \end{aligned}$$



The total velocity potential at P due to the entire line distribution is

$$\phi = \int_0^{2l} \frac{m dx}{r} = m \int_0^{2l} \frac{dx}{\sqrt{d^2 + (x_1 - x)^2}} = -m \left[\text{Sinh}^{-1} \left(\frac{x_1 - x}{d} \right) \right]_0^{2l}$$

$$= -m \left[\text{Sinh}^{-1} \left(\frac{x_1 - 2l}{d} \right) - \text{Sinh}^{-1} \left(\frac{x_1}{d} \right) \right]$$

$$= -m \left[\text{Sinh}^{-1} \left(\frac{x_2}{d} \right) - \text{Sinh}^{-1} \left(\frac{x_1}{d} \right) \right] \rightarrow (i)$$

Consider $\text{Sinh}^{-1} \left(\frac{x_2}{d} \right) = y$,

$$\frac{x_2}{d} = \text{Sinh } y = \frac{e^y - e^{-y}}{2}$$

$$\frac{2x_2}{d} = e^y - e^{-y}$$

$$\frac{2x_2}{d} = e^y - \frac{1}{e^y}$$

$$\frac{2x_2 e^y}{d} = e^{2y} - 1$$

$$e^{2y} - \frac{2x_2}{d} e^y - 1 = 0$$

$$e^y = \frac{\frac{2x_2}{d} \pm \sqrt{\left(\frac{2x_2}{d}\right)^2 - 4(1)(-1)}}{2(1)}$$

$$= \frac{x_2 \pm \sqrt{x_2^2 + d^2}}{d}$$

Take log,

$$y = \log \left[\frac{x_2 \pm \sqrt{x_2^2 + d^2}}{d} \right]$$

$$\sinh^{-1} \left(\frac{x_2}{d} \right) = \log \left| \frac{x_2 + \sqrt{x_2^2 + d^2}}{d} \right|$$

$$\text{iii) } \ln \sinh^{-1} \left(\frac{x_1}{d} \right) = \log \left(\frac{x_1 + \sqrt{x_1^2 + d^2}}{d} \right)$$

$$(i) \Rightarrow \phi = -m \left[\log \left(\frac{x_2 + \sqrt{x_2^2 + d^2}}{d} \right) - \log \left(\frac{x_1 + \sqrt{x_1^2 + d^2}}{d} \right) \right]$$

$$= m \left[\log \left(\frac{x_1 + \sqrt{x_1^2 + d^2}}{d} \right) - \log \left(\frac{x_2 + \sqrt{x_2^2 + d^2}}{d} \right) \right]$$

$$= m \log \left[\frac{\frac{x_1 + \sqrt{x_1^2 + d^2}}{d}}{\frac{x_2 + \sqrt{x_2^2 + d^2}}{d}} \right] = m \log \left[\frac{x_1 + \sqrt{x_1^2 + d^2}}{x_2 + \sqrt{x_2^2 + d^2}} \right]$$

$$= m \log \left[\frac{x_1 + \sqrt{r_1^2}}{x_2 + \sqrt{r_2^2}} \right] = m \log \left(\frac{x_1 + r_1}{x_2 + r_2} \right)$$

$$\text{Now, } r_1^2 - x_1^2 = r_2^2 - x_2^2 = d^2$$

$$(r_1 - x_1)(r_1 + x_1) = (r_2 - x_2)(r_2 + x_2) = d^2$$

$$\frac{r_1 + x_1}{r_2 + x_2} = \frac{r_2 - x_2}{r_1 - x_1} = \frac{r_1 + x_1 + r_2 - x_2}{r_2 + x_2 + r_1 - x_1} = \frac{r_1 + r_2 + 2l}{r_1 + r_2 - 2l}$$

At P on the Spheroid through P having A, B as foci
 $r_1 + r_2 = 2a$

$$\text{Hence } \frac{r_1 + x_1}{r_2 + x_2} = \frac{r_2 - x_2}{r_1 - x_1} = \frac{2a + 2l}{2a - 2l} = \frac{a+l}{a-l}$$

$$\phi = m \log \left(\frac{r_1 + x_1}{r_2 + x_2} \right) = m \log \left(\frac{a+l}{a-l} \right) \quad \text{--- (*)}$$

The equipotentials are given by $\phi = \text{constant}$

$$m \log \left(\frac{a+l}{a-l} \right) = \text{constant}$$

$$\frac{a+l}{a-l} = \text{constant} \Rightarrow a = \text{constant}$$

i.e. $\frac{r_1 + r_2}{2} = a = \text{constant}$

$$r_1 + r_2 = \text{constant}$$

These Surfaces are confocal ellipsoids of revolution about AB with A, B as foci. Let P be any point on the ellipsoid specified by parameter a, P' a point on the neighbouring ellipsoid specified by parameter (a + da), where $\overline{PP'} \equiv \delta n$.

Then the Velocity at P is

$$\vec{v} = -\nabla \phi = -\frac{\partial \phi}{\partial n} \hat{u}$$

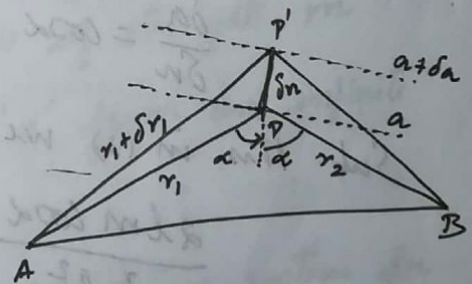
$$= -\frac{\partial}{\partial n} \left\{ m \log \left(\frac{a+l}{a-l} \right) \right\} \hat{u}$$

$$= -m \frac{\partial}{\partial n} \left\{ \log(a+l) - \log(a-l) \right\} \hat{u}$$

$$= -m \hat{u} \left\{ \frac{1}{a+l} - \frac{1}{a-l} \right\} \frac{\partial a}{\partial n}$$

$$-\nabla \phi = -m \hat{u} \left\{ \frac{a-l - a-l}{(a+l)(a-l)} \right\} \frac{\partial a}{\partial n}$$

$$-\nabla \phi = -m \hat{u} \left(\frac{-2l}{a^2 - l^2} \right) \frac{\partial a}{\partial n} = \frac{2lm}{a^2 - l^2} \frac{\partial a}{\partial n} \hat{u} \quad \text{--- (2)}$$



Now the normal at P bisects 2α , the angle between the focal radii AP, PB.

From $\triangle APP$

$$(r_1 + \delta r_1)^2 = r_1^2 + (\delta n)^2 - 2 r_1 \delta n \cos(\pi - \alpha)$$

$$= r_1^2 + \delta n^2 + 2 r_1 \delta n \cos \alpha$$

$$(r_1 + \delta r_1) = (r_1^2 + \delta n^2 + 2 r_1 \delta n \cos \alpha)^{1/2}$$

$$\approx r_1 + \delta n \cos \alpha$$

Similarly from $\triangle BPP$

$$(r_2 + \delta r_2) = (r_2^2 + \delta n^2 + 2 r_2 \delta n \cos \alpha)^{1/2}$$

$$r_2 + \delta r_2 \approx r_2 + \delta n \cos \alpha$$

Adding we get

$$r_1 + \delta r_1 + r_2 + \delta r_2 = r_1 + r_2 + \delta n \cos \alpha + \delta n \cos \alpha$$

$$r_1 + \delta r_1 + r_2 + \delta r_2 - r_1 - r_2 = 2 \delta n \cos \alpha$$

$$\delta r_1 + \delta r_2 = 2 \delta n \cos \alpha$$

$$\rho \delta a = 2 \delta n \cos \alpha$$

$$\frac{\delta a}{\delta n} = \cos \alpha$$

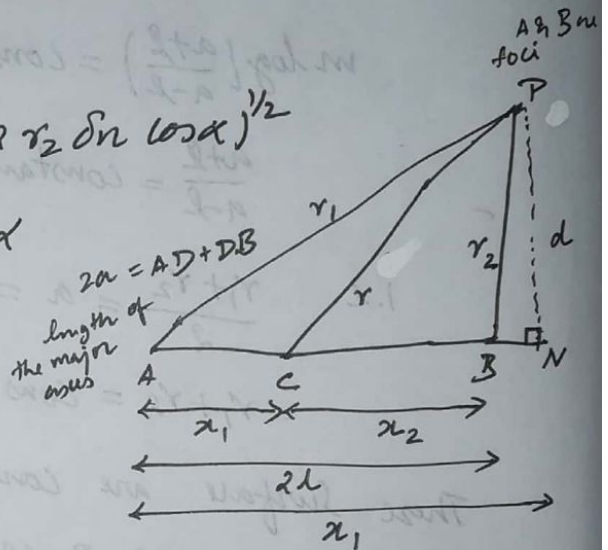
Sub. this in (2) we get

$$\frac{2 \rho m \cos \alpha}{a^2 - b^2} \hat{i}$$

Hence the velocity at P is $\frac{2 \rho m \cos \alpha}{a^2 - b^2} \hat{j}$

Images in a Rigid infinite plane

Suppose a surface S can be drawn in a moving fluid in such a way that there is no transport



of fluid across S . Let S divide the fluid into two regions labelled 1, 2. Then any system of the sources, sinks (or) doublets in 2 is called an image system of the regions in S .

If we remove the fluid in 2 and replace S by a rigid boundary of the same size and shape, then the flow in 1 is unaltered in accordance with the conditions of the uniqueness theorems.

It follows, then, that if we know the image system for 1 in S , we can solve the problem of flow in 1 against a rigid surface S .

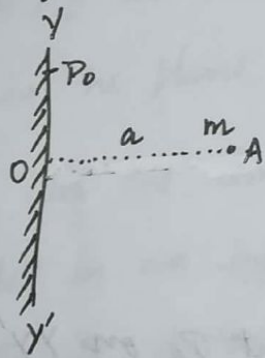


Fig (i)

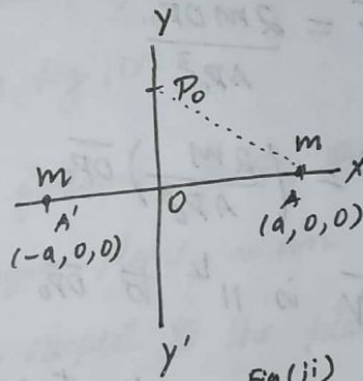


Fig (ii)

Fig (i) shows a simple source of strength 'm' situated at a distance 'a' from an infinite rigid plane YY' .

We first show that the appropriate image system for this is an equal source at A' , the optic image of A in the plane.

Consider fig (ii) in which we have equal sources of strength m at $A(a, 0, 0)$ and $A'(-a, 0, 0)$.

Let P_0 be any point on the plane YY' in

Fig (ii) then the fluid velocity at P_0 is,

$$\vec{q} = \frac{m}{AP_0^2} \cdot \hat{AP}_0 + \frac{m}{A'P_0^2} \cdot \hat{A'P}_0$$

$$= \frac{m}{AP_0^2} \cdot \hat{AP}_0 \cdot \frac{AP_0}{AP_0} + \frac{m}{A'P_0^2} \cdot \hat{A'P}_0 \cdot \frac{A'P_0}{A'P_0}$$

$$= \frac{m}{AP_0^3} \cdot \overline{AP}_0 + \frac{m}{A'P_0^3} \cdot \overline{A'P}_0$$

$$= \frac{m}{AP_0^3} (\overline{AP}_0 + \overline{A'P}_0)$$

$$= \frac{m}{AP_0^3} (\overline{AO} + \overline{OP}_0 + \overline{A'O} + \overline{OP}_0)$$

$$= \frac{m}{AP_0^3} (\hat{a} + \overline{OP}_0 - \hat{a} + \overline{OP}_0)$$

$$\vec{q} = \frac{2m\overline{OP}_0}{AP_0^3}$$

$$\vec{q} = \left(\frac{2m}{AP_0^3} \right) \overline{OP}_0$$

$$\Rightarrow \vec{q} \text{ is } \parallel \text{ to } \overline{OP}_0$$

This shows that at any point P_0 on YY' , the fluid flows tangentially to the plane YY' . Thus there is no transport of fluid across this plane.

Thus in fig (ii) at all corresponding points P_0 on the surfaces YY'

$$\vec{q} \cdot \hat{n} = 0$$

$$-\nabla\phi \cdot \hat{n} = 0$$

$$\Rightarrow \frac{\partial\phi}{\partial n} = 0 \text{ for the region of flow } x \geq 0$$

By uniqueness theorem, that the image of m at A in YY' in Fig (i) is m at A' , the optic image of A in

yy'

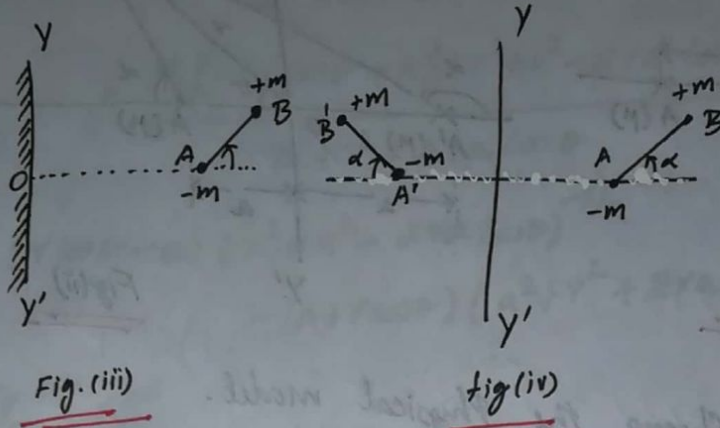


Fig. (iii)

fig (iv)

Consider a pair of sources $-m$ at A , m at B close together and on one side of the rigid plane yy' in fig (iii).

The image system is $-m$ at A' , m at B' , where A' , B' are the respective optic images of the point A , B in the plane yy' in fig (iv).

In the limit it follows, then, the image of a doublet in an infinite rigid plane is an equal doublet symmetrically disposed with respect to the plane.

Example

- 1) A three-dimensional doublet of strength μ whose axis is in the direction \vec{ON} is distance ' a ' from the rigid plane $x=0$ which is the sole boundary of liquid of density ρ , infinite in extent. Find the pressure at a point on the boundary distant r from the doublet given that the pressure at infinite is P_0 . Show that the pressure on the plane is least at a distance $a\sqrt{5}/2$ from doublet.